

Alicyclobacillus acidoterrestris spores as a target for Cupuaçu (*Theobroma grandiflorum*) nectar thermal processing: kinetic parameters and experimental methods

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Abstract

The kinetic parameters of thermal inactivation of a spore former, *Alicyclobacillus acidoterrestris*, in a tropical fruit nectar [25% of Cupuaçu (*Theobroma grandiflorum*) pulp and 15% sugar] were determined by the isothermal method (IM), under batch heating, and by the paired equivalent isothermal exposures (PEIE) method, under non-isothermal continuous conditions. The isothermal experiments were repeated three times, every 4 months, with the same spore suspension kept frozen between experiments. The aging of spores, under frozen storage, seemed to produce a notorious increase in the z -value from experiment to experiment: Experiment 1 ($z = 7.8 \pm 2.6$ °C, $D_{95}^{\circ\text{C}} = 5.29 \pm 0.96$ min), Experiment 2 ($z = 22 \pm 5$ °C, $D_{95}^{\circ\text{C}} = 5.99 \pm 0.63$ min), and Experiment 3 ($z = 29 \pm 10$ °C, $D_{95}^{\circ\text{C}} = 3.82 \pm 0.48$ min). The evaluation of the kinetic parameters by the PEIE method was carried out in parallel with Experiment 3, with the same aged spores, and the results ($z = 31 \pm 6$ °C, $D_{95}^{\circ\text{C}} = 5.5 \pm 1.2$ min) were close to the ones obtained in this experiment. From this work, it seems that the PEIE method can also be applied to evaluate the reduction parameters of a spore-forming microorganism, and in a more realistic way, since the continuous system eliminates the errors caused by come-up and cool-down times (CUT and CDT) that are unavoidable in isothermal experiments. Therefore, when designing a thermal process for a continuous system, the PEIE method should be used, or the chances are that the process would be underdesigned, risking that the desired level of spore inactivation would not be achieved. An optimization of the thermal processing conditions was next performed for Cupuaçu nectar, considering a $5D$ reduction in *A. acidoterrestris* spores. If a pasteurization process is considered, the conditions that ensure safety (9 min at 98 °C) only allow a 55% retention of ascorbic acid (AA). If sterilization is considered, 8 s at 115 °C will ensure a safe product and retain 98.5% of the original ascorbic acid. Therefore, if *A. acidoterrestris* is considered as the target microorganism, the nectar should undergo an aseptic high temperature short time principle (HTST) process to achieve a $5D$ reduction in this acidophilus spore former. However, if the hot-fill-and-hold pasteurization process is preferred, the product should be fortified with ascorbic acid.

Keywords: *Alicyclobacillus acidoterrestris* spores; Inactivation kinetics; PEIE method; Isothermal method; Cupuaçu (*Theobroma grandiflorum*) nectar

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1. Introduction

When designing a thermal process to produce shelf stable juices or nectars (which usually have low pH, $\text{pH} < 4.5$), *Clostridium botulinum* is not a concern since it is generally accepted that the spores of this microorganism will not grow or produce toxin at $\text{pH} < 4.6$ (Blocher and Busta, 1983). Yeast, molds, and some nonspore-forming bacteria (e.g. *Lactobacillus plantarum*) are therefore, the most probable spoilage flora. To destroy this flora, a pasteurization process is enough and acid fruit juices have been processed for years by hot-fill-and-hold pasteurization systems. The product is heated to approximately 90–95 °C during a holding time of approximately 15–20 s, followed by a cooling period until 82–84 °C, before filling the product into the package. Next, it is held hot for about 2 min before the packages are cooled down in a cooling tunnel (Solberg et al., 1990). However, in the 1980s, the fruit juice industry started facing a serious problem: consumer complains about spoiled juices long before their shelf life had expired. An off flavor and sometimes loss of color were the main complaints (Walls and Chuyate, 1998). As no gas production was reported, in some cases, it was thought to be a chemical contamination, but with time, it was concluded to be due to microbial growth (Walls and Chuyate, 1998). Only a spore former could survive a thermal treatment in the pasteurization range, and it had to be acidophilic to grow in acid juices. There was already some evidence that acidophilic spore formers existed, such as *Bacillus coagulans*, known to spoil tomato paste and juice (York et al., 1975; Rodrigo et al., 1990; Sandoval et al., 1992). The microbial growth on apple juice was isolated and identified as a new type of spoilage bacterium (Cerny et al., 1984), and named by Deinhard et al. (1987) as *B. acidoterrestris*. Later, it was reclassified as a new genus *Alicyclobacillus*, becoming *Alicyclobacillus acidoterrestris* (*A. acidoterrestris*), which together with *A. acidocaldarius* and *A. heptanicus* had in common the presence of a ω -alicyclic fatty acid as the major fatty acid in the cell membrane (Yamazaki et al., 1996). Closely packed rings of this fatty acid form a protective coating to the cellular membrane, explaining the resistance of these three microorganisms to acid environments (Pontius et al., 1998; Walls and Chuyate, 1998).

The effect of different acids (citric, tartaric, and malic acids) on the heat resistance of *A. acidoterrestris* spores was studied in model systems by Pontius et al. (1998). No significant differences were shown in the temperature range studied (91–100 °C), although the type of acid seemed to have a more severe effect at temperatures below 91 °C. Soluble solids (Brix) concentration had a major influence on growth (Splittstoesser et al., 1994). It was reported that for white grape juice made from Riesling grapes, a 19.2° Brix would inhibit growth, whereas 18.2° Brix would be the optimum value for growth to occur. Silva et al. (1999) developed a predictive model for *D* values as a function of pH, soluble solids, and temperature of the environment. A recommendation about redesigning thermal processes for juices, endangered by this microorganism, was made by Pontius et al. (1998), and for new fruit juices or juice mixes, this acidophilic spore former should become a concern.

The design of a thermal process should include an optimization, in order to make sure that the level of inactivation, required for the target microorganism, is satisfied without impairing the quality of the food product. An optimization process involves several factors (Teixeira and Shoemaker, 1989): (1) an objective function, which in thermal processing is usually identified as the maximization of a quality attribute; (2) decision variables, adjustable and with an independent nature. These are variables that affect the value of the objective function. In thermal processing, they are specific of the process model, e.g. temperature of heating fluid, flow rate of product to be processed, etc.; (3) a set of constraints allowing the decision variables to take certain values, but not others, to deal with equipment limitations. They can also be imposed by safety requirements, e.g. level of reduction on a microorganism in order to keep the product safe; (4) a process mathematical model, since process simulation allows prediction of the objective function by constraining the decision variables; and (5) the optimization technique to be chosen. If only a few variables are defined, producing a limited number of solutions, a very simple optimization technique can be used based on a search for the best solution that best satisfies the requirements imposed by the objective function in the mathematical model.

For the reasons mentioned above and considering the pH and Brix of the Cupuaçu nectar ($\text{pH} \approx 3.2$ and

18° Brix), *A. acidoterrestris* was considered a target microorganism for the design of a thermal process for this product. The main objectives of the work presented in this article were: (i) to model the thermal inactivation kinetics of *A. acidoterrestris* spores in Cupuaçu (*Theobroma grandiflorum*) nectar using two methods, the isothermal method (IM) and the paired equivalent isothermal exposures (PEIE) method (Welt et al., 1997; Vieira et al., 2000, 2001); (ii) to optimize the thermal process conditions, maximizing ascorbic acid (AA) retention of the product.

1.1. Theoretical considerations

Destruction of microorganisms does not imply physical destruction, but loss of viability (maybe due to the inactivation of an enzyme) (Geankoplis, 1993). First-order kinetics can represent the death-rate behavior of microorganisms,

$$C = C_0 e^{-kt} \quad (1)$$

where C_0 is the initial concentration, C is the concentration at time t , k is the rate constant, and t is the time of thermal exposure.

Thermobacteriologists prefer to describe microorganisms thermal inactivation first order reaction kinetics in terms of decimal logarithmic reduction (Eq. (2)) (Stumbo, 1973; Etsy and Myer, 1922; Geankoplis, 1993),

$$N = N_0 10^{-(t/D_T)} \quad (2)$$

where N_0 is the number of initial microbial population and N is the number of survivor microbial population at a given time. The thermal reduction time (D), defined by microbiologists as the time it takes for a population of microorganisms to be reduced by 90%, is related to the rate constant (k) (Geankoplis, 1993),

$$D = \frac{2.303}{k}. \quad (3)$$

The temperature dependency of the rate constant (k) can be described by the Bigelow model (Bigelow, 1921),

$$D_T = D_{T_{\text{ref}}} 10^{-(1/z)(T - T_{\text{ref}})}. \quad (4)$$

The isothermal method (IM) (Lenz and Lund, 1980) is not ideal for estimation of thermal kinetic parameters of reactants because of unavoidable errors caused by come-up and cool-down times. Swartzel (1982) developed the equivalent point method (EPM), one of the first methods implemented to overcome this problem. In this method, a G value was first introduced which is a function of the time–temperature history $T(t)$ (Swartzel, 1982),

$$G = \frac{\ln \frac{C}{C_0}}{-k_0} = \int_0^t \exp\left(-\frac{E_a}{RT(t)}\right) dt \quad (5)$$

where k_0 (min^{-1}) is the rate constant at infinite reference temperature, E_a (kJ/mol) is the activation energy, and R is the universal gas constant.

This method postulated that in continuous heating, depending on the E_a values (different activation energies) and G values (different thermal exposures), different lines would be produced all intersecting in one point, the equivalent point, defined by an equivalent time and temperature (t_E , T_E), equivalent isothermal exposure,

$$G = t_E \exp\left(-\frac{E_a}{RT_E}\right). \quad (6)$$

However, deviations to this intersection were verified (Maesmans et al., 1995; Welt et al., 1997). In order to avoid this problem, new methods were developed based on modifications on EPM, such as the line intersection (LI) method (Kyereme et al., 1999) and the paired equivalent isothermal exposures (PEIE) method. The latter, being iterative, gives at the end of the iterative procedure an equivalent isothermal exposure (EIE) for each combination (T_E and t_E are determined by solving Eqs. (7a) and (7b), simultaneously):

$$\ln t_E = \ln G_1 + \frac{E_{a1}}{RT_E} \quad (7a)$$

$$\ln t_E = \ln G_2 + \frac{E_{a2}}{RT_E}. \quad (7b)$$

The corresponding isothermal rate constants, k_E 's, are next determined for each thermal exposure,

$$k_E = -\frac{\ln(C/C_0)_{\text{exp}}}{t_E}. \quad (8)$$

An Arrhenius curve is then obtained by plotting $\ln k_E$ vs. $1/T_E$, where the slope gives a new E_{a_i} and the y-intercept, the k_{ref} (dynamic set). The generation of a new E_{a_i} , as a multiple or submultiple of E_{a_i} , initiates a new iteration. This iterative procedure continues until there is no difference between the dynamic sets obtained in two consecutive iterations.

The PEIE method can be slightly modified to apply the Bigelow model (Bigelow, 1921). The corresponding isothermal D values, D_E 's, are then determined for each thermal exposure,

$$D_E = -\frac{t_E}{\log(N/N_0)} \quad (9)$$

and from a plot of $\log D_E$ vs. T_E , the final z-value will be obtained.

$$z = \frac{T_{E1} - T_{E2}}{\left(\log \frac{D_{E2}}{D_{E1}}\right)} \quad (10)$$

2. Materials and methods

2.1. Cupuaçu nectar preparation

Frozen Cupuaçu pulp was imported from Brazil in 1-kg bags. A nectar with a composition of 25% Cupuaçu, 15% sugar, 50% water, and 10% of a spore suspension containing 10^5 *A. acidoterrestris* spores/ml was prepared. Before adding the spore suspension, the mixture was homogenized with a Moulinex Turbomix 2 blender, for 3 min and passed through a plastic strainer. In order to define the initial population, appropriate dilutions were then made in order to enumerate the spores by the method described below.

2.2. Suspension of *A. acidoterrestris* spores

A spore suspension of *A. acidoterrestris*, strain NCIMB 13137 (National Collections of Industrial and Marine Bacteria, Auris Business Centre, Aberdeen, UK), was prepared by adding a portion of freeze-dried spores, previously produced by Silva et al. (1999), to a flask containing 200 ml of sterile water and glass beads. The suspension was then kept in the cold at 4 °C and shaken several times a day in order to

destroy clumps before proceeding to enumeration. A 10^{-1} -dilution was then done, to obtain 100 ml of a working solution, and the original suspension was frozen and stored in a freezer at -18 °C.

2.3. Enumeration of spores

The spores were first observed by phase contrast microscopy. A great majority of the spores were refringent. Then, using a Newerbauer chamber, the concentration of the suspension was determined by direct microscopy count. The counting was performed five times and the results were averaged. The spores were also enumerated using the method developed by Pettipher et al. (1997): 0.1 ml spread onto orange serum agar (OSA) (Merck) plates, followed by incubation at 44 °C for 48 h. Although this method had been optimized for a different strain, *A. acidoterrestris* 2498, recovery of the strain used in this study (NCIMB 13137) was very good as well.

2.4. Modeling the kinetics of thermal inactivation of *A. acidoterrestris* spores

2.4.1. Isothermal experiments

For each thermal treatment, 2-ml vials (Chrom-pack) were filled with the inoculated nectar, sealed, and placed in a rack. Next, they were immersed in an oil bath (Grant W38) preset at the desired temperature for the thermal treatment. The vials were taken out of the oil bath, after the required holding time, and immediately cooled down to 4 °C in an iced water bath to stop the heat treatment immediately. Five temperatures were studied (90, 95, 100, 105, and 110 °C) for holding times ranging from 0 to 40 min. After the thermal treatment, from each vial, appropriate dilutions were made to enumerate the survivor population by the method described above. As vials were used, instead of capillary tubes, it was not expected that the studied temperatures would be instantly reached. To obviate this problem, a replicate study was carried out with thermocouples placed within the vials of spore suspension for the purpose of determining the come-up time (CUT). Zero time and the corresponding initial count were considered only after the CUT. This procedure had the advantage of heat shocking the spores and freeing the nectar from any vegetative cells present during the CUT.

However, additional lethality contributed during cool-down times (CDT) could not be considered. Three isothermal studies were carried out with the same spore solution, Experiment 1—right after rehydration, Experiment 2—4 months after frozen storage, and Experiment 3—8 months after frozen storage. Between studies, the spore solution was kept frozen in a freezer at $-18\text{ }^{\circ}\text{C}$. Before each experiment, the spores were observed microscopically and spore enumeration was performed as described above.

2.4.2. Dynamic thermal treatments

Seven different thermal exposures were applied to Cupuaçu nectar. The tests were conducted under nonuniform heating conditions, using the same spore suspensions as in IM Experiment 3 (after 8 months of frozen storage). A plate heat exchanger and a holding tube were used (Armfield Pasteuriser FT-43A), as described in Vieira et al. (2001). In order to produce different t_E and T_E , different processing temperatures and flow rates were used. The pasteurizer had 32 plates in the heating section and the holding tube was composed of three sections, immersed in a water bath set at the temperature needed. Before, and between runs, the whole system was sanitized by running a hypochlorite solution (500 ppm) for 15 min, followed by running hot water at $95\text{ }^{\circ}\text{C}$ for 10 min (procedure described by Wescott et al., 1995). For each run, three samples were collected, each in decontaminated flasks.

2.5. Time–temperature history

In order to obtain the time–temperature history, an element of volume dv was dyed with a 2% (w/v) solution of methylene blue, by injecting 1 ml at the entrance of the feeding tube at time 0. The temperature changes in dv were monitored along the pathway by inserting TCT thermocouples between the pasteurizer plates on the product side and at the entrance and exit of each holding tube section and cooling tube. The temperature data were recorded by a data acquisition system (Delta Logger devices). The corresponding traveling time of dv (from the entrance to each site of insertion of a thermocouple) was recorded using a stopwatch and visual detection of the blue dyed nectar, following the method described in Vieira et al. (2001).

2.6. Data analysis

The kinetic data obtained in the isothermal experiments were analyzed using the isothermal method (IM). A one-step nonlinear regression to all the data, using the software STATA (Stata Corporation, 1995), was carried out as described in Vieira et al. (2000).

A FORTRAN program was developed ‘Kinprmb-glow’, to apply the PEIE method step by step (Welt et al., 1997; Vieira et al., 2001) using the Bigelow model.

The following modifications were introduced:

1. after the stabilization of the iterations, the D_E values were calculated from the EIE data (T_E and t_E) and experimental thermal destruction of *A. acidoterrestris* spores (Eq. (9));
2. from a plot of $\log D_E$ vs. T_E , the final z -value and D_{ref} were obtained (Eq. (10)).

3. Results and discussion

3.1. Spore enumeration

The spores enumerated by direct count (1.95×10^6 c.f.u./ml) were just slightly lower (but not significantly different) than the number counted by spread plating (2.00×10^6 c.f.u./ml). However, in most cases, the opposite occurred because usually a small percentage of the spores was not viable and therefore, could be seen with a microscope and directly counted, but did not grow in any media (not counted by spread plating). According to Bourgeois and Malcoste (1995), the number of counts in counting chambers should be three. In this particular case, although five counts were used, the existence of clumps might have caused this behavior.

3.2. Isothermal method (IM)

The results obtained from the isothermal experiments (Fig. 1) were well fitted by the Bigelow model (Eq. (4)). The kinetic parameters, z and $D_{95\text{ }^{\circ}\text{C}}$, obtained, using a one-step nonlinear regression, are presented in Table 1 for each isothermal study (Experiments 1, 2, and 3).

The z -value for Experiment 1 is in agreement with the already published z -values for other strains of this

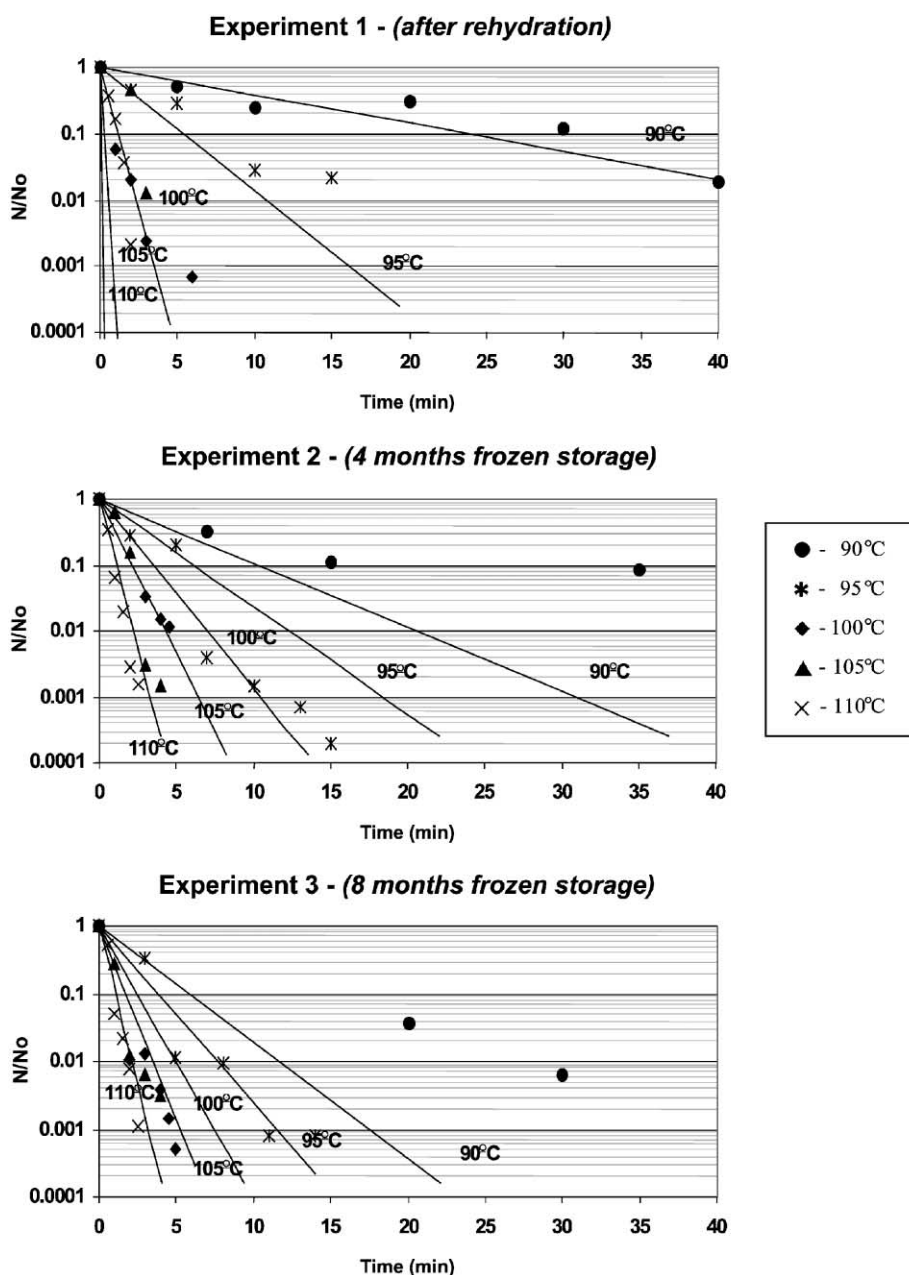


Fig. 1. Effect of temperature and time on the degradation of *A. acidoterrestris* spores in Cupuaçu nectar (pH 3.2 and 18° Brix).

microorganism in fruit juices, especially with the ones by Eiroa et al. (1999) and Splittstoesser et al. (1994) (Table 2). Concerning the *D* values, a higher value is obtained for the Cupuaçu nectar (Table 1), which might be a result of the higher soluble solids content.

Experiments 2 and 3 were meant to confirm the results of the first study. However, it was verified that the behavior of the spores changed considerably. The spores' thermal degradation sensitivity to temperature changes decreased from Experiment 1 to Experiment 3,

Table 1

Thermal reduction kinetic parameters for *A. acidoterrestris* spores in Cupuaçu nectar, using the isothermal method (IM) (18° Brix, pH 3.2)

	Isothermal method		
	Experiment 1 (after rehydration)	Experiment 2 (4 months frozen storage)	Experiment 3 (8 months frozen storage)
$D_{95} \text{ }^{\circ}\text{C}$ (min)	5.29 ± 0.96	5.99 ± 0.63	3.82 ± 0.48
z ($^{\circ}\text{C}$)	7.8 ± 2.6	22 ± 5	29 ± 10
R^2	0.97	0.97	0.98
No. of observations	25	27	26

as it can be observed by the increase in the z -value (Table 1). This behavior might have been caused by the aging under frozen storage between the experiments. So far, no studies were reported on the influence of frozen storage on the behavior of the spores of *A. acidoterrestris*. Alpin and Hodges (1979) reported the influence of storage temperature on the spores of a different microorganism, *B. stearothermophilus*, but they observed a different behavior. The spores of this *Bacillus* species, when stored at -18°C , exhibited a loss in viability and heat resistance after 8 days of storage. Food safety considerations would dictate that thermal process design be based upon the worse case

possible for spores found in nature. Therefore, the highest z -values (least temperature sensitivity) should be adopted for this purpose.

3.3. PEIE method

In Fig. 2, the thermal profiles from the seven dynamic experiments are presented, and the corresponding inactivation data of *A. acidoterrestris* spores are shown in Table 3. These results were used in the PEIE method to evaluate the kinetic parameters. Although 21 combinations were expected, giving 42 data points, 10 combinations were lost. This fact is

Table 2

Thermal inactivation kinetic parameters of several strains of *A. acidoterrestris* spores in different juices

Juice	Strain	SS	pH	Temperature ($^{\circ}\text{C}$)	D value (min)	z -Value ($^{\circ}\text{C}$)	Reference
Apple		nr ^a	3.51	80	41.15 ± 0.24	12.2	Komitopoulou et al., 1999
				90	7.38 ± 0.85		
				95	2.30 ± 0.03		
Grapefruit	Z CRA 7182	nr ^a	3.42	80	37.87 ± 0.20	11.6	
				90	5.95 ± 0.32		
				95	1.85 ± 0.05		
Orange		nr ^a	3.90	80	54.30 ± 0.42	12.9	
				90	10.30 ± 0.30		
				95	3.59 ± 0.04		
Orange	DSM2498	nr ^a	nr ^a	85	$50.00 \pm \text{nr}$	7.9	Eiroa et al., 1999
				90	$16.90 \pm \text{nr}$		
				95	$2.70 \pm \text{nr}$		
Apple	VF	11.4	3.50	85	56.00 ± 14.00	7.7	Splittstoesser et al., 1994
				90	23.00 ± 7.50		
				95	2.80 ± 0.70		
Grape	WAC	15.8	3.30	85	57.00 ± 13.00	7.2	
				90	16.00 ± 4.10		
				95	2.40 ± 0.90		
Cupuaçu extract	NCIMB 13137	11.3	3.60	85	17.50 ± 1.10	9.0	Silva et al., 1999
				91	5.35 ± 0.57		
				95	2.82 ± 0.27		
				97	0.57 ± 0.03		

^a nr—not reported.

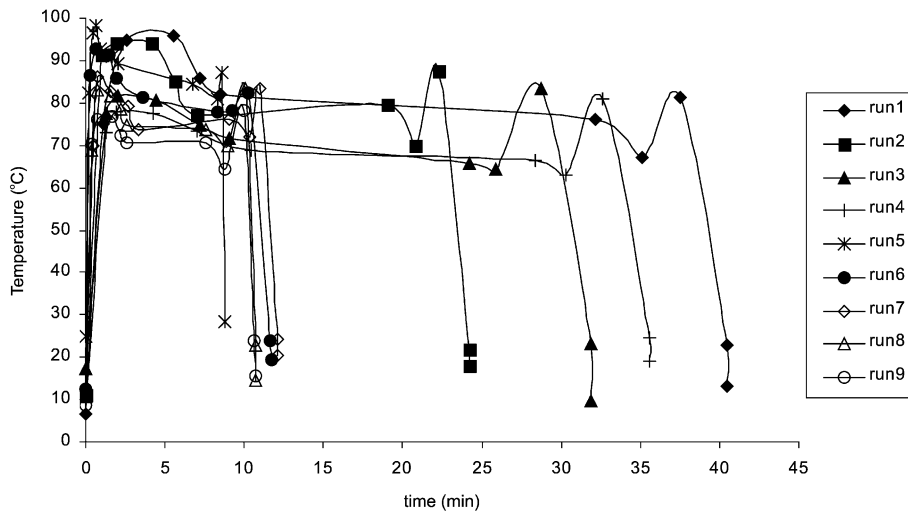


Fig. 2. Time-temperature histories for all seven runs.

explained by the presence of combinations that either lead to negative values of E_a (if in a combination, $T_{E1} < T_{E2}$ and $k_{E1} > k_{E2}$, or vice versa) or to E_a values too high or too low, when compared to the average values (existence of very close values of T_E or t_E) (Welt et al., 1997). By applying the Bigelow model to the data obtained (D_E 's and corresponding T_E 's) and through regression analysis (Fig. 3), a z -value of 31 ± 6 °C and a D_{95} °C of 5.5 ± 1.2 min were obtained (Table 4, Fig. 3). Both the R^2 of 0.87 and the residuals analysis performed (Fig. 4) indicated that the regression line obtained, with the estimated parameters, presented a good fit. Residuals higher than 0.2 were considered as outliers and were discarded. The inactivation data predicted by the model is also

presented in Table 3 and compared with results from isothermal Experiment 3.

Comparison of Table 1 (Experiment 3) and Table 4 shows that the results obtained from both methods are close, although for the PEIE method (continuous system), both the z -value and the D_{95} °C were higher. This behavior can be interpreted as a consequence of failure to account for added lethality contributed to cool-down time that could not be accounted for in isothermal experiments, especially at higher temperatures when lethality occurs very rapidly in a short time. This difference in z -values, between isothermal and continuous methods, was already noticed on other occasions (Table 5).

Table 3
Experimental final reduction of *A. acidoterrestris* spores in Cupuaçu nectar for all continuous thermal treatments

Run #	Flow rate (l/h)	Maximum temperature reached (°C)	N/N_{0exp}	N/N_{0pred}
1	0.28	99	0.012	0.002
2	0.46	95	0.037	0.023
3	0.4	85	0.067	0.080
4	2.9	99	0.083	0.120
5	0.3	80	0.118	0.100
6	2.8	90	0.254	0.280
7	2.8	85	0.123	0.350

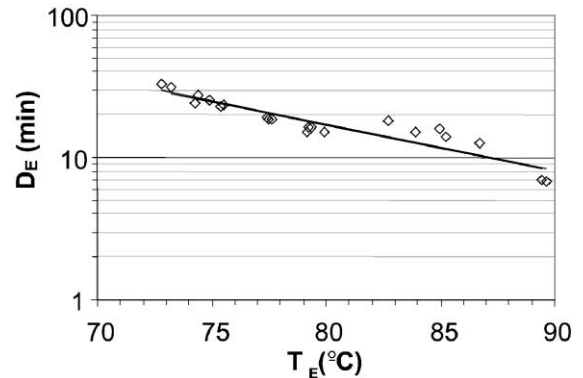


Fig. 3. PEIE Bigelow plot, obtained using all seven dynamic thermal treatments, after 12 iterations.

Table 4

Kinetic parameters of thermal inactivation of *A. acidoterrestris* spores in Cupuaçu nectar (18° Brix, pH 3.2) using the PEIE method and Experiment 3 of the IM method

	PEIE method	IM Experiment 3
$D_{95} \text{ }^{\circ}\text{C} \text{ (min)}$	5.5 ± 1.2	3.82 ± 0.48
$z \text{ (}^{\circ}\text{C)}$	31 ± 6	29 ± 10
R^2	0.87	0.98
No. of observations	22	26

As mentioned above, in the isothermal study, the increase in the z -value from experiment to experiment was probably due to spore injury caused by being frozen under storage, 4 months from Experiment 1 to Experiment 2 and then another 4 months to Experiment 3. Again, for purposes of food safety, this must be assumed indicative of the heat resistance exhibited by these spores when found in nature.

3.4. Optimization of thermal process

The objective function in this study is to maximize the retention of ascorbic acid, AA, having as decision variables: (i) the steam pressure that affects the heating fluid temperature (in this case water) and (ii) the flow rate of the Cupuaçu nectar, which will directly affect the holding time. A 5D reduction in *A. acidoterrestris* spores was imposed as a constraint (FDA, 1998). This optimization was only possible because of the different kinetic parameters for both AA and *A. acidoterrestris* spores, as generally, bacteria have lower z -values (much more heat sensitive to temperature changes) compared with quality parameters. Therefore, an increase in temperature will benefit retention of quality parameters for the same level of

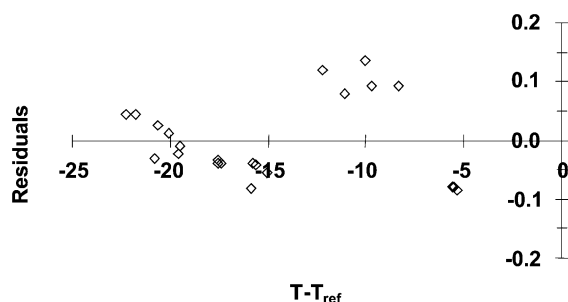


Fig. 4. Residuals analysis of the regression of D_E vs. T_E .

Table 5

z -values determined using a batch and a continuous system

Reference	z -value ($^{\circ}\text{C}$)		Type of microorganism
	Batch	Continuous	
Bunning et al., 1988	7 ^a	7.3	<i>Listeria</i>
Fairchild et al., 1994	4.8 ^a	5.9	<i>Listeria innocua</i>
		8.2 ^b	<i>Bacillus cereus</i>
		8.5 ^c	
Wescott et al., 1995	8.5 ^a	7.5 ^b	<i>Bacillus stearothermophilus</i>
	8.1 ^a	7.3 ^c	
Mackey and Bratchel, 1989	6.1 ^a	7.4	<i>Listeria monocytogenes</i>

^a Capillary tube method.

^b Traditional method.

^c Equivalent point method.

inactivation in bacteria (HTST—high temperature short time principle) (Holdsworth, 1985).

A simple optimization technique was chosen: a search for the best time–temperature combinations that would maximize the retention of AA, keeping the level of inactivation of *A. acidoterrestris* spores (5D). Fig. 5 is a semilogarithmic plot of time vs. temperature where thermal degradation lines for AA (dashed lines) are superimposed on a thermal death time (TDT) curve for *A. acidoterrestris* spores (thick line) (Teixeira and Shoemaker, 1989). The dashed lines, obtained from the kinetic data of thermal degradation of AA evaluated (Vieira et al., 2001) using the PEIE method, represent time–temperature combinations that keep a retention of 55–98.5% of AA. The coarse line 1 (constraint) was obtained from the kinetic data for *A. acidoterrestris* spores using the isothermal method (Table 1, Experiment 1) for illustrative purposes. Unfortunately, the kinetic data from the PEIE method (IM Experiments 2 and 3 as well) produced z -values ($z = 30 \text{ }^{\circ}\text{C}$) close to those for AA degradation ($z = 38 \text{ }^{\circ}\text{C}$). Under these conditions, there would be limited opportunity for optimization. Coarse line 1 (Fig. 5) represents time–temperature combinations that yield a 5D reduction in *A. acidoterrestris* spores (assuming a z of $7.8 \text{ }^{\circ}\text{C}$). From the interception of the coarse line 1 with the dashed lines, two thermal treatments are obtained: (A) in the pasteurization temperature range (with 55% AA retention): $98 \text{ }^{\circ}\text{C}$ during 9 min, and (B) in the sterilization temperature range (98.5% AA retention): $115 \text{ }^{\circ}\text{C}$ during 8 s. It

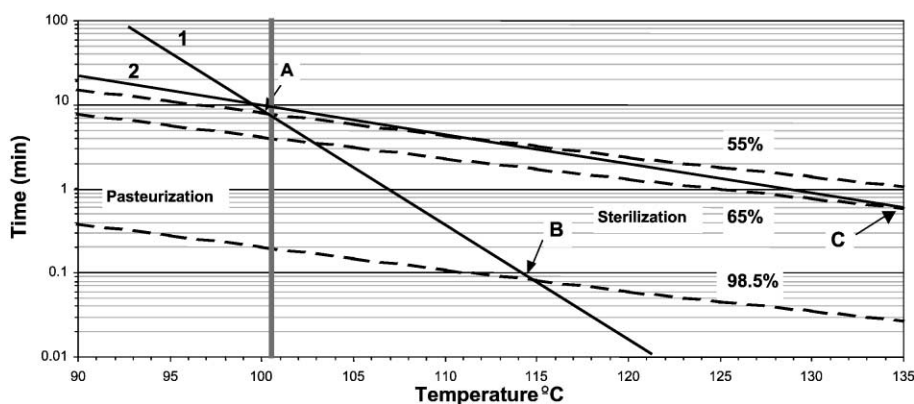


Fig. 5. Graphical optimization for thermal processing of Cupuaçu nectar. Coarse lines 1 and 2 are both for a 5D reduction on *A. acidoterrestris* spores, assuming $z = 7.8$ °C and $z = 30$ °C, respectively, and the three dashed lines are from top to bottom, respectively, for 55%, 65%, and 98.5% AA retention. A vertical gray line separates the pasteurization from sterilization range of temperatures. The arrows indicate the three optimal time–temperature combinations: (A) 9 min, 98 °C; (B) 8 s, 115 °C; and (C) 36 s, 135 °C.

should be noted that these conditions do not apply if process designs were to be based upon the worse case z -values of 29–30 °C for aged spores, as shown in coarse line 2 for illustrative purposes. In this case, the best ascorbic acid retention would be expected to be 65% or less to satisfy the 5D constraint under feasible time–temperature conditions, as this line intercepts the *A. acidoterrestris* coarse line 2 at 135 °C and 36 s (Fig. 5, point C).

4. Conclusions

From this work, it seems that the PEIE method can also be applied to estimate the thermal inactivation kinetic parameters of a spore-forming microorganism in a more realistic way. Therefore, when designing a thermal process for a continuous system, the PEIE method should be used to estimate the reduction kinetic parameters (if instantaneous heating and cooling are not possible with traditional isothermal experiments), or chances are, that the process would be underdesigned, risking that the desired spore population reduction would not be achieved.

If *A. acidoterrestris* spores are considered as the target microorganisms, then it is recommended that Cupuaçu nectar should undergo an aseptic HTST process in the sterilization temperature range to achieve a 5D reduction. However, if the hot-fill-and-

hold pasteurization process is preferred (because it can be a more appropriate and simple technology), then the product should be fortified with ascorbic acid, or packaged with minimum headspace to limit the availability of oxygen that is needed in order for the degradation reaction to proceed.

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